

ALPHA 10/10P SERVICE MANUAL**CIRCUIT DESCRIPTION**

The mother PCB is common for both the A10 and A10P with the exception of the input mode switch and pre-amp output mute relay which are only fitted to the A10 and the power/standby LED and links to parallel the input connections to what would otherwise be the pre-amp output for use with a mono link. The amplifier is based on the D290/Alpha 9 design but with lower gain, a higher current and higher voltage driver stage and a high power output stage. The current servo has been improved over the Alpha 9 to be output device independent. A micro supervises the amplifier state, switch state and remote control functions. Provision is made for an additional 3rd channel PCB to be added with power supply and protection circuitry access.

Input stage

The input connections are taken either from the pre-amp connector, LK12X, or the external power amp input on the A10 depending on the position of SW1. On the A10P, the input is taken from the external power amp input only with provision for a mono shorting link by having two parallel input connectors. On the A10, there is a mute relay on the pre-amp outputs which are always connected to the pre-amp connector, LK12X.

The signal is passed through a low pass filter with a -3dB point of 550KHz at normal gain and 740KHz at low gain. The gain is selected by SW2. C72 and C74 are d.c. blocking capacitors with a -3dB point of 0.7Hz. A d.c. error correction current is injected into the base of Q19 and 26 from the voltage servo Z3 and 4, to null any voltage offset at the amplifier output.

The input and voltage amplifier stages both run off regulated 15 Volt supplies. The input stage is an NPN differential input, Q18, 19, 25 and 26, with an adjustable current source, Q21 and 28 which sets the quiescent current through all the stages but specifically the output stage. C37, R58, C49 and R66 keep the input stage and voltage amplifier stable. Q52, 53, 54 and 55 form a current mirror to ensure that the differential input is balanced during normal operation.

Voltage Amplifier

The voltage amplifier consists of another differential pair, Q48, 49, 50 and 51. Q48 and 50 are the positive pulling side of the voltage amplifier output and Q49 and 51 pull negative via a current mirror Q8, 9, 10 and 11. The network C12, 36, R74 and 77 give the current mirror gain to compensate for the fact that Q49 and Q51 is only driven from the low-impedance side of the input stage current mirror. The network ensures a fast, symmetrical slew rate of the voltage amplifier stage.

Network C69, 70, R172, 174 ensure the overall stability of the amplifier by reducing the open loop gain at high frequencies.

Second Voltage Amplifier and Driver Stage

Q33, 36, 41 and 44 are the next voltage amplifier stage with feedback applied from the output coupled to their emitters. This stage runs on the full supply rail voltages and splits the level shifts the signal via Q2, 3, 5 and 6 to drive the gates of the output MOSFETs, Q13, 14, 15 and 16. Q2 and 3 simply buffer the inverted signal at the collector of Q36 to drive the low side MOSFETs, Q13 and 15. Q5 and 6 invert the inverted signal at the collector of Q41 and Q44 to drive the high side MOSFETs, Q14 and 16. To ensure that the high side drive is able to swing far enough to ensure the high side MOSFETs can be driven to saturation, a bootstrap, C5, D41 R57, C78 and D22 boosts the driver stage power supply during positive excursions of the amplifier output. This is inactive at low output voltage swings as any distortion induced by the network would be more audible at such levels.

Output Stage

Both the high and low side output devices feature over-current protection, Q17, 23, 24, 30 which clamps the gate of the MOSFET it protects. A high current is permitted through the MOSFET for a few milliseconds after which time the current is throttled down to about 10A peak. A second current sensing network, Q32 and Q35 activates the over-current protection cut-out if the low side is current limiting for too long, a few hundred milliseconds. The current sensing resistors do not reduce the transconductance of the MOSFETs because the driver stage is referenced to the MOSFET source. This means that the current through the driver stage is also sensed but this is insignificant as far as over-current protection sensing is concerned.

Auto-bias

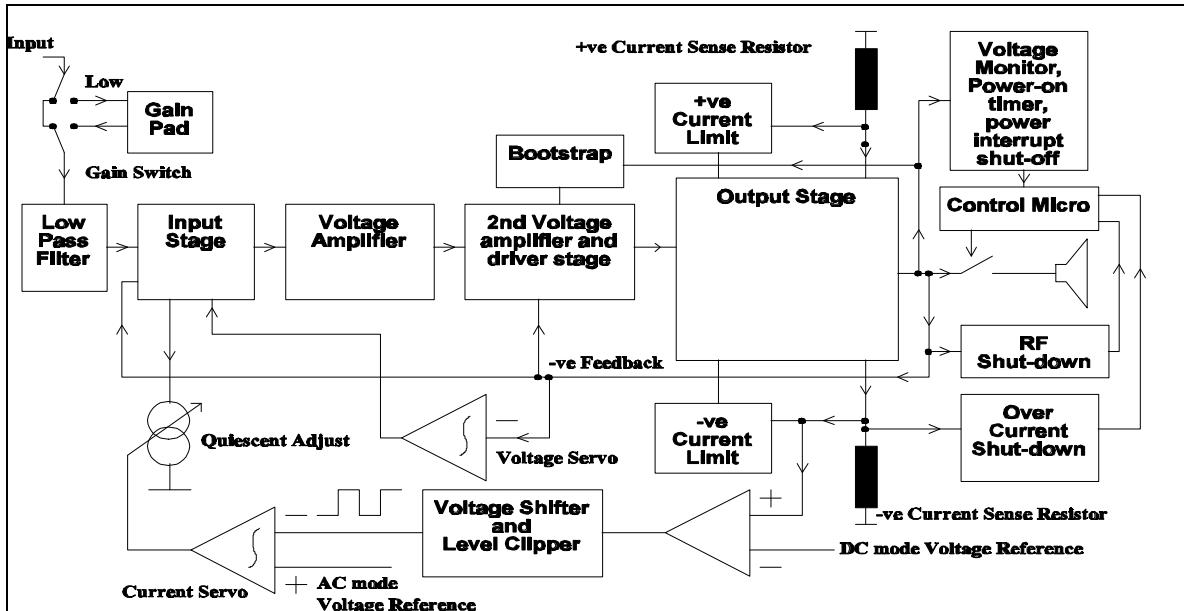


Figure 1 Block Diagram of Power Amplifier

The bias is regulated in two modes, one where there is no signal and one when signal is being split between the high and low side MOSFETs when driving a alternating signal into a load.

Under static conditions, Z8 simply compares the sensed current, which includes the driver stage current, with a d.c. mode reference of 13mV. The sense resistor is 0.11 so this corresponds to a current of about 120mA, some of which is driver current. The current through the MOSFETs is about 80mA at this point. The comparator output is level shifted to drive the integrating current servos Z3 and 4. This adjusts the amplifier current so that, on average, the bias level is held at the reference point.

Under dynamic conditions, the low side drive will definitely be conducting more current than the reference (80mA) for half the signal cycle and will be switched off for the other half. The result is a rectangle wave output from the comparator, Z4.

When the output stage is biassed correctly (class AB operation) the comparator output toggles when the current through the sense resistor for the -ve MOSFET is equal to the d.c. mode static reference level and at the half way point of the signal. The result is a perfect square wave output from the comparator. Under these conditions, the +ve MOSFET is also conducting the same amount of current at this point. If the bias level is lower than the reference, say, at zero (class B operation) then the -ve MOSFET will spend slightly less than half the time conducting at or above the reference level resulting in a rectangle wave output from the comparator at a duty cycle slightly less than 50%. If the bias level is higher than the reference then the -ve MOSFET will spend slightly more than half the time conducting at or above the reference level resulting in a rectangle wave output at a duty cycle slightly more than 50%. The change in duty cycle away from 50% causes the integrator, Z3 and Z4 to adjust the bias level via the bias adjusting transistors, Q22 and 29.

The integrator has a reference, the a.c. mode dynamic reference, for a bias point slightly higher than for a 50% duty cycle. This eliminates the possibility of the bias being slowly throttled due to component tolerance mismatch resulting in a reference which would pull the servo down. A high dynamic bias reference level simply stabilises the bias slightly higher than the static reference but a low dynamic reference causes the bias to drift down to complete throttle.

This system works if the signal is a.c., symmetrical and is not a rectangle wave. Certainly, only a.c. signals are passed

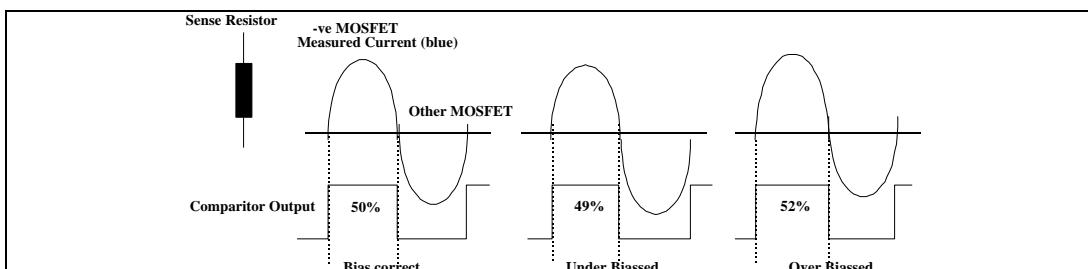


Figure 2 Auto-bias under dynamic conditions

through the amplifier due to C72 and 74 d.c. blocking capacitors and on average the signal will be symmetrical. Any short-term asymmetry will be ironed out by the long time constant of the integrator.

Main Power Supply

The main power supply is regulated in two stages. First it is pre-regulated by Q1 and 4 to about 11V less than the main supply rails. This supply is made available to an option board. The maximum load on these supplies is 150mA for less than 2W dissipation in Q1 and 4. These supplies are then regulated to +/-15V by Z1 and 2. These supplies are used by the input stages of the power amplifiers including any 3rd channel board, the pre-amplifier board and an optional phono amplifier board. The positive voltage regulator, Z1, has a larger heatsink than Z2 because the phono board consumes much more current from the positive rail than from the negative rail.

Control Micro

The control micro performs the following functions...

- ◆ Switches the amplifier on or off,
- ◆ Mutes the speakers #1 or #2 or the pre-amp output,
- ◆ Monitors the heatsink temperature,
- ◆ Monitors RF content of speaker outputs,
- ◆ Handles the remote bus and infra red remote input,
- ◆ Reports fault conditions to the main display and LED,
- ◆ Reads the speaker and power switch positions.

The control micro runs of the constant power supply from standby transformer, TX2. This enables the amplifier to be switched on or off remotely from the remote bus or, in the case of the integrated amplifier, from an infra red remote control. This power supply is intended to supply all the digital circuitry in the amplifier including any option boards. This is supplied at 8V to the other boards where it will be locally regulated to 5V as required.

The micro communicates with the display board via a multi-master I²C bus. This bus is used to report amplifier and power status to the display micro and remote control commands received. It is also possible for the display micro to control functions on the power amplifier board. The option board also uses this bus to receive any remote control commands and communicate with the display micro.

The external remote bus handles raw information from infra red sensors with no demodulating. The remote bus input can be echoed to the output through a buffer circuit. The incoming signal is demodulated by Z13. Raw signal is also sent to the micro interrupt line, pin 12, for assessing the noise on the remote bus. In addition, any d.c. signal on the remote bus is sensed on pin 2 of the micro in when it is not being used as an output to mute the hardware remote echo buffer. The micro must modulate any output it sends to this bus with a carrier (37KHz). The output will drive one or two series infra red LEDs directly.

The list below shows how various fault conditions can be deduced simply from the Power LED behaviour.

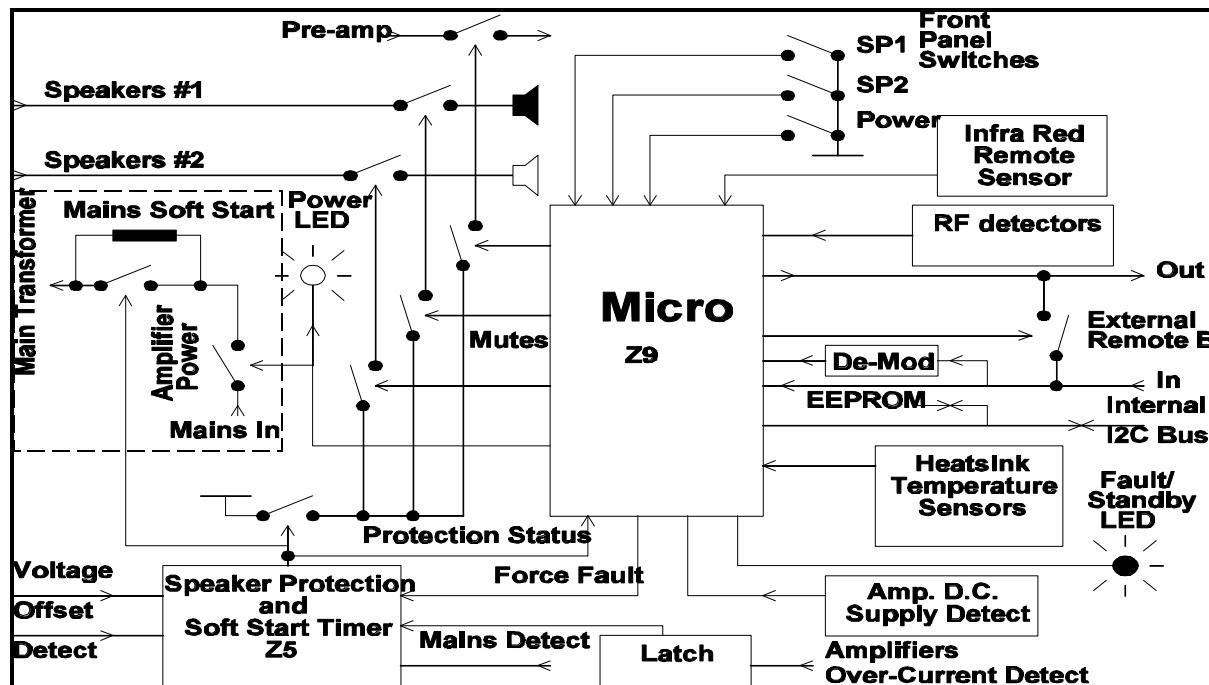
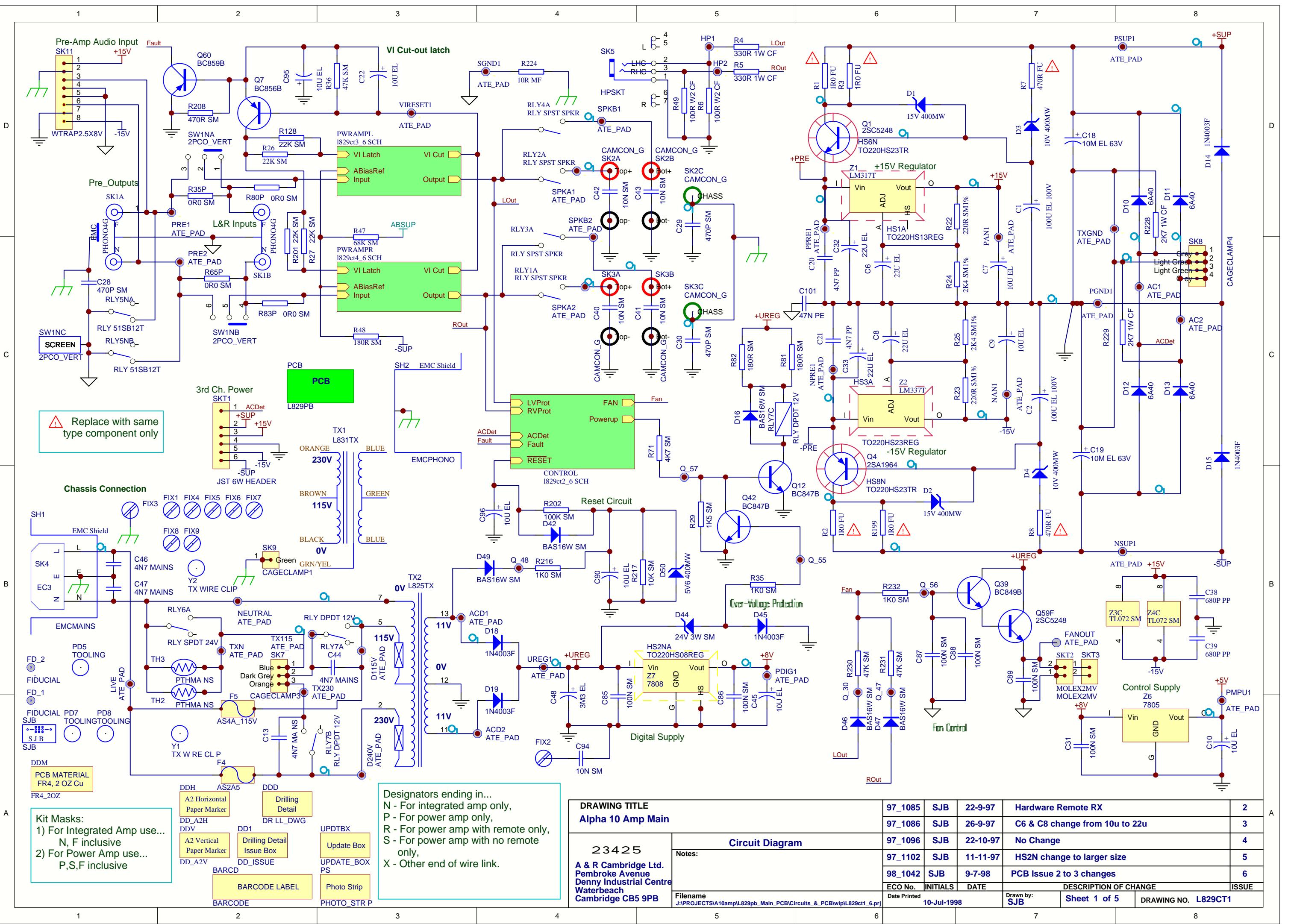
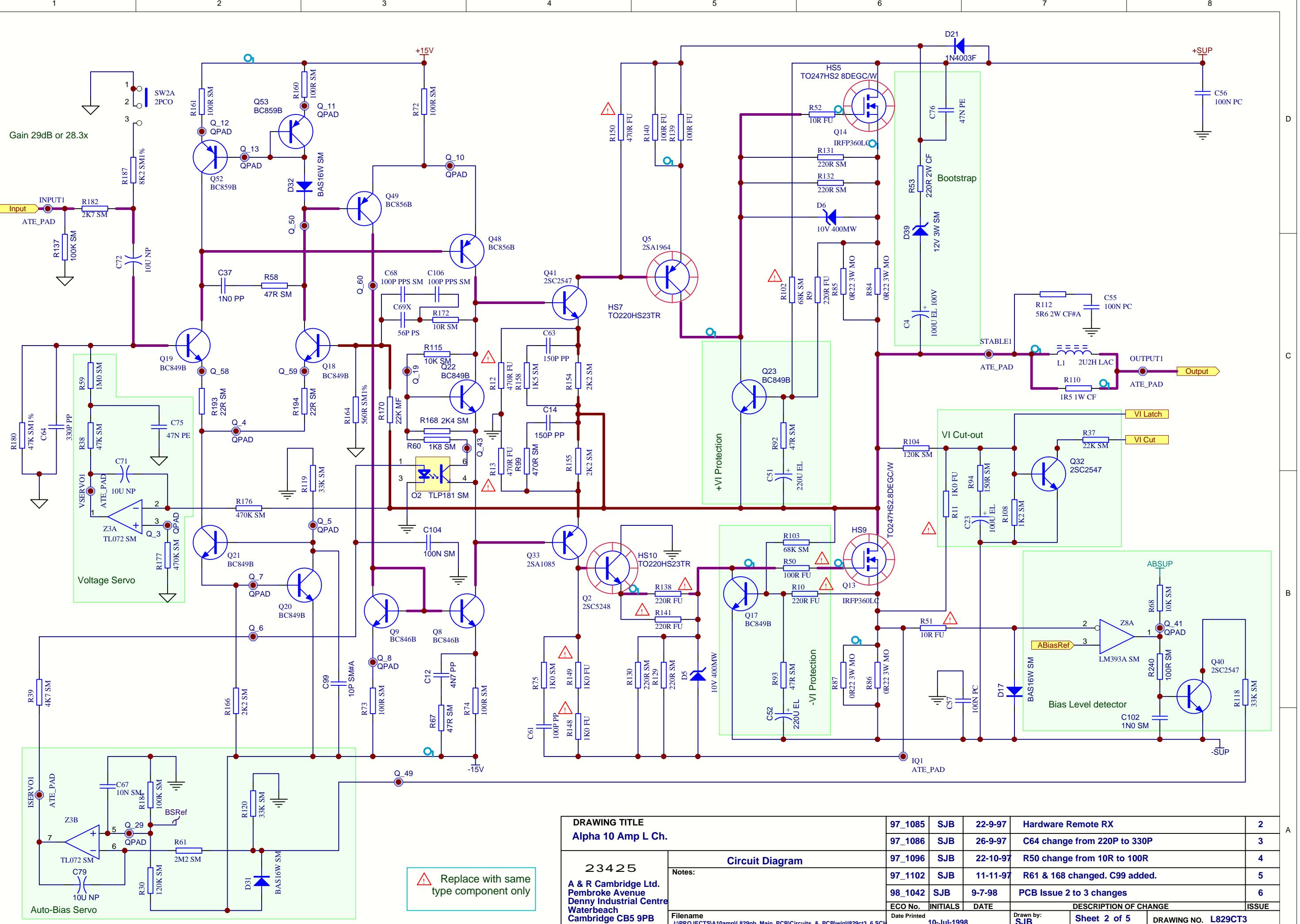
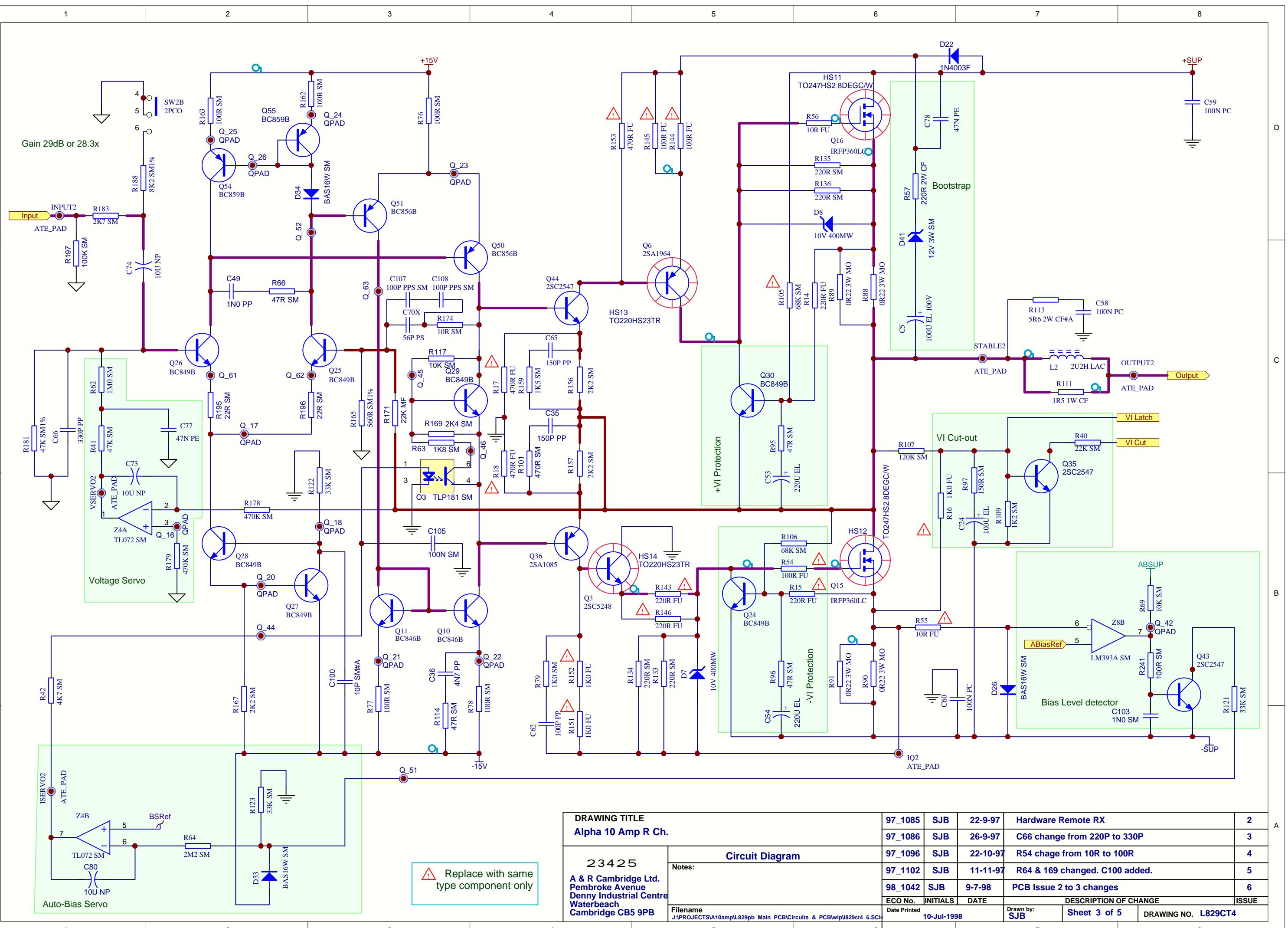
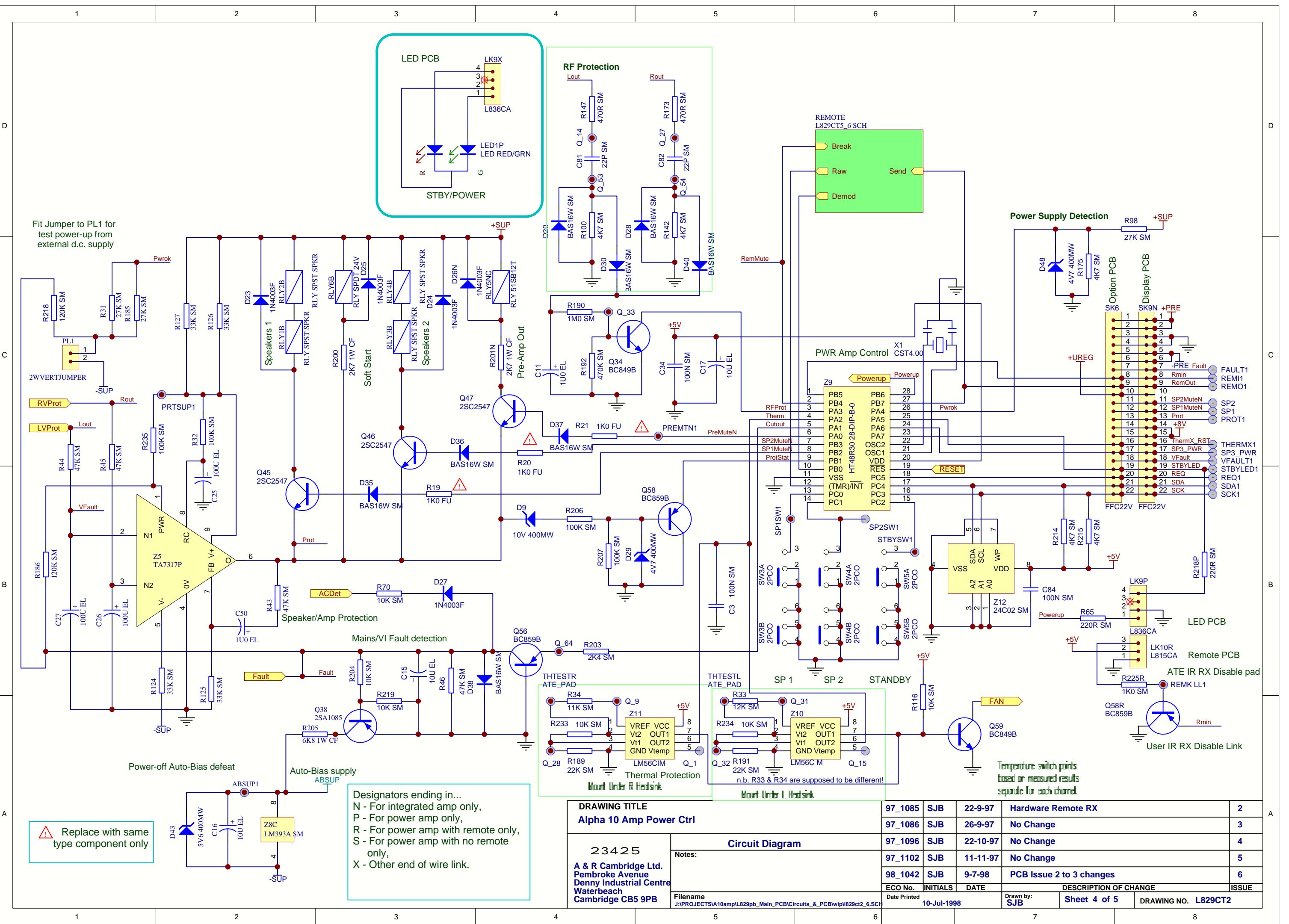


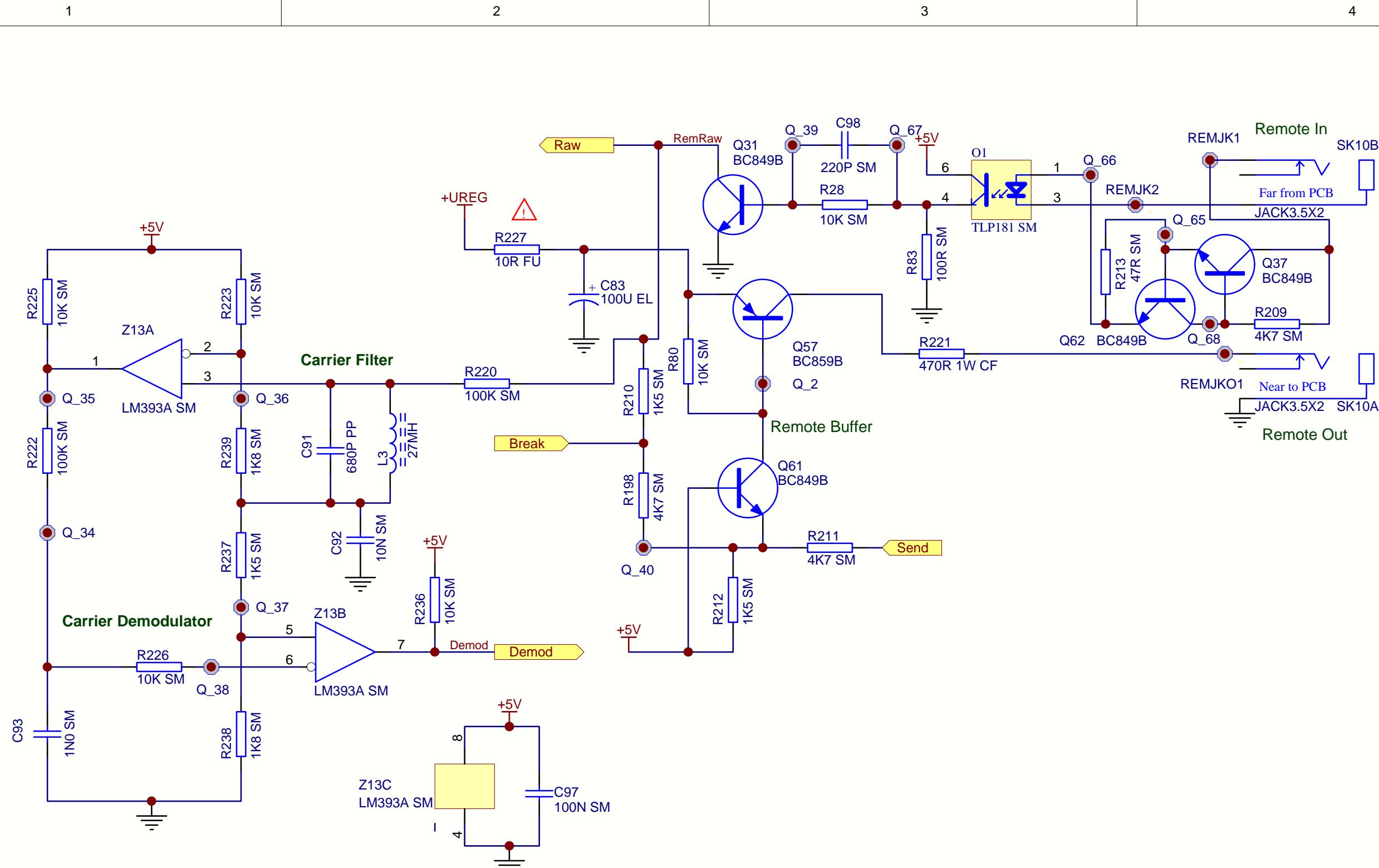
Figure 3 Micro Block Diagram











A	23425 A & R Cambridge Ltd. Pembroke Avenue Denny Industrial Centre Waterbeach Cambridge CB5 9PB	DRAWING TITLE Alpha 10 Amp Remote Bus			97_1085	SJB	22-9-97	Hardware Remote RX	2
		Circuit Diagram			97_1086	SJB	26-9-97	No Change	3
		Notes:			97_1096	SJB	22-10-97	R210, R198, R212 change	4
					97_1102	SJB	11-11-97	No Change	5
					98_1042	SJB	9-7-98	PCB Issue 2 to 3 changes	6
		Filename J:\PROJECTS\A10amp\L829pb_Main_PCB\Circuits_&_PCB\wip\L829CT5_6.SCH	Date Printed 10-Jul-1998	ECO No.	INITIALS	DATE	DESCRIPTION OF CHANGE		

