Service Manual

FMJ P7 7-Channel Amplifier

Contents List

Front panel **Front**

Rear panel the contract of the Chassis **and Chassis** and Chassis and Chas

 TX tray $-$

Technical Specifications

Contents

- ! **Technical specifications**
- ! **Rear panel silk screen**

Technical Specifications

All measurements are with 230V/50Hz mains power

Amplifier Board L924

Contents

- ! **Circuit description**
- ! **Component overlay**
- ! **Parts list**
- ! **Circuit diagrams**

P7 Amplifier Module

Circuit Description Refer to L924 circuit diagrams

Introduction

L924 is the power amplifier module for the P7 multichannel amplifier. There are 7 identical modules in the P7. The circuit design is based on the A85 / A32 output stage topology. The main features of the amplifier module are as follows:

- Preset 'THX' gain (29dB closed loop gain). 0dBV input signal corresponds to 100 watts into 8Ω output power
- Capable of producing 150 watts of sinusoidal output power into an 8Ω resistive load (with greater than 250W into 3.2Ω subject to thermal dissipation limits)
- Relay coupled output for silent power on / off and load protection
- Opto-isolated fault and control lines to the microprocessor PCB (to avoid hum loops and instability, to improve EMC performance and crosstalk)
- DC coupled signal path with integrating servo to remove residual DC errors
- Instantaneous load protection
- Mono block design (each channel is electrically isolated from all others and has independent power supply windings on the mains transformer)
- Integrated modular heatsink for good thermal performance and ease of assembly / servicing
- Low harmonic and intermodulation distortion
- Flat frequency response
- Fast (and symmetrical) slew rate
- High damping factor
- Unconditionally stable into loads of up to $\pm 90^\circ$ phase angle

Sheet 1

The input to the amplifier is connected via SK103. The 2 phono sockets are connected in parallel to allow 'daisychaining' of amplifier modules. R104 provides a DC leakage path to the chassis (i.e. mains power earth) to prevent small transformer leakage currents causing the electrical 0V of the amplifier to rise significantly above mains earth potential. C104 provides an EMC coupling between the local input ground and the chassis to reduce common mode RF noise.

Star point SP101 connects the differently named electrical 0V nets at a single point. This is to ensure the correct wiring topology of the ground connections on the printed circuit board. SP101 provides a good common ground reference point when making voltage measurements on the PCB. Note that 0V_DIG is *not* connected to SP101, as this is the microprocessor ground.

Relay RLY101 connects the output of the amplifier to the load via socket SK105.

L101 and R103 form part of a 'Zobel' network to decouple the load at high frequencies to ensure amplifier stability into capacitive loads.

Note that signals 6 through 9 are open collector outputs. active low, referred to 0V_DIG with no pull-up resistors. This is because they are wire OR'd on the microprocessor PCB (L925), where the pull-up resistors to +5V digital are located.

The line 'NFB' provides for a portion of the negative feedback of the amplifier to be taken on the load side of RLY101. The components that allow for this (R236 thru R239) are not presently fitted, meaning that RLY101 is not included in the feedback loop.

SK104 connects to the microcontroller PCB. Note that all signals on this connector are electrically isolated from the amplifier circuit itself, via either opto isolators or the relay coil of RLY101. The 10 pin connector has the following signals:

SK104

Sheet 2

Port INPUT connects the input of the amplifier, referred to 0V_SIG, which is the precision signal ground reference.

Zener diodes DZ202 and DZ203 limit the input signal amplitude to approximately 5.3Vpk. This is to prevent damage to the input of opamp IC200, due to a leaky source signal or electrostatic discharge.

R223, R228 and C210 form a passive $1st$ order low pass filter with a – 3dB corner frequency of roughly 330kHz to prevent ultrasonic signals from entering the circuit and possibly causing damage.

The main amplifier circuit is a 'classic' current feedback design.

IC200A is configured as a non-inverting amplifier with a gain of 2. Its purpose is to provide current outputs (via its power supply pins) and a current input (via its output pin). This forms the voltage to current (transimpedance) conversion and phase splitting necessary to drive the voltage gain stage. The 'current feedback' occurs because when IC200 drives its 44Ω load to ground, the power supply pin currents are half-wave rectified versions of the drive current of the amplifier. This causes voltage gain, which is buffered and passed on to the outputs. The feedback from the output to pin 1 of IC200 acts to reduce the gain of the amplifier; when this current is roughly equal to the current required to drive the input signal into 44Ω , equilibrium is reached and the closed loop gain is defined. The output stage provides the vast majority of the current required to drive the 44Ω signals to ground. The op-amp only provides a very small error current sufficient to give the required voltage magnification.

Transistors TR204 and TR203 are wired as cascodes (common base amplifiers). Their purpose is to provide IC200 with ±15V power supply rails, whilst allowing IC200's power supply pin currents to pass through them to the NPN and PNP current mirrors.

The resistor, zener diode and capacitor circuits on the bases of TR204 and TR203 are to provide a controlled ramp up during power on, a stable power supply voltage and good local HF decoupling.

Transistors TR200, TR201 and TR202 form a PNP Wilson current mirror. Likewise TR205, TR207 and TR206 form an NPN Wilson current mirror. The outputs of these two current mirrors are connected together via the bias network around TR212.

The two current mirrors combine to provide a very high-gain current to voltage (transresistance) gain stage, which provides all the voltage gain of the amplifier (roughly 80dB at low frequency).

C205, C207, R221 and R222 provide the loop compensation for the amplifier. They combine to produce an open-loop pole at roughly 10kHz and a corresponding open-loop zero around 500kHz. This allows for good time domain performance and clean square wave reproduction. The amplifier is designed to be critically damped. There should be no ringing or overshoot apparent on the output signal when a (small) step function is applied to the input.

Diodes D200 and D202 act to limit the current through TR202 and TR206 in the event of a fault condition. When the input current exceeds 14mA the diodes conduct and the transresistance stage becomes a constant current source, killing the open loop gain and preventing damage to the transistors.

Resistors R219 and R220 decouple the supplies for the amplifier gain stages from the main power rails. This is to permit the bootstrap circuit to modulate these supplies, increasing efficiency. The bootstrap will be described in more detail later.

TR212 provides a 4.7V bias voltage to allow the following pre-driver stage to operate in class 'A'. It also acts as a V_{BE} multiplier for TR209 and TR214 to maintain an approximately constant current as the ambient temperature inside the box changes.

TR209 and TR214 form a class 'A' pre-driver emitter follower stage to boost the current gain and isolate the transresistance stage from the output transistors. This is important to keep the loop gain of the amplifier high and thus minimise distortion. TR208 and TR213 act as a current limit (roughly 30mA) to prevent the destruction of TR209 and TR214 in a fault condition.

R247, R248, R249 and R250 are to loosely decouple the emitters of TR209 and TR214 from the output stage. This is very important. The output devices (Sanken power Darlingtons) have inbuilt temperature compensating diodes which control the bias voltage to their bases. Each output device has a 150Ω resistor so that the inbuilt diodes can accurately control quiescent V_{BE} and hence collector current as the output power and device temperature varies. Preset potentiometer RV200 adjusts the quiescent current. *NB Ensure that the amplifier has fully warmed up before adjusting the quiescent current.* D201 protects the output devices from destruction in the event of the preset potentiometer going open circuit. PL200 allows the test engineer to measure the bias voltage (and thus collector current).

C217, C218, C220 and C221 provide local HF stability around the output transistors to prevent parasitic oscillation. D204 and D205 are catch diodes to reduce the effects of induced back-EMF in the loudspeaker load.

R254 and C223 form part of the 'Zobel' network that ensures the amplifier sees a constant load of roughly 4.7Ω at very high frequencies. This helps to improve stability and reduce HF output noise.

C208 and C209 provide local high frequency decoupling for the output devices.

IC200B forms the DC integrating servo. Its purpose is to remove residual DC errors due to slight device mismatch and component tolerances. It is configured as an inverting integrator with a time constant of 0.47 seconds. Any positive DC offset at the output of the amplifier will cause the output of the op-amp to go negative, increasing the current in the negative supply pin and thus 'pulling' the output down to ground (and vice versa). D203 protects the inverting input of IC200B in a fault condition.

The bootstrap circuit consists of C213, C214, R241, R242, R219 and R220. The purpose of the bootstrap is to allow the output voltage swing to modulate the power supply rails of the input and voltage gain stages. This allows this circuit's power supply voltage to exceed the main power rails connected to the output devices, allowing the driver stage to fully drive the output and thus give the best thermal efficiency. The 'bottom' of R219 sees a peak-to-peak voltage swing of approximately 15 volts at full output power (i.e. it goes 7.5 volts above the rail at the peak of the cycle). The 'top' of $\overline{R220}$ should see the same voltage swing.

Sheet 3

This sheet contains the protection circuits and interface to the microprocessor signals.

TR309, TR305 and their associated components form the instantaneous load protection circuit for the output transistors. They sense the voltage across the 0.22Ω emitter resistors (hence emitter current) and the collector-emitter voltage, cutting off the base drive to the output transistors when the collector current or device power dissipation exceeds a preset limit.

The protection circuit is designed to allow large (unrestricted) currents into loads of 3Ω and above but limit the current into a short circuit or very low impedance load. C318, C319, R335 and R336 form a 2.2ms time constant, which will allow larger transients of current delivery for a few milliseconds, to ensure that the amplifier has a sufficiently large transient capability to drive 'difficult' loudspeaker loads with a music signal.

TR311 also turns on when the protection circuit activates. This switches on optocoupler IC300B causing a fault signal to be transmitted to the microcontroller. The microcontroller will then switch off the output relay to protect the amplifier.

TR310, TR302 and their associated components form the DC offset detection circuit. A positive DC offset at the output will turn on TR310. A negative DC offset at the output will turn on TR302, thus causing TR313 to turn on. In either case optocoupler IC300A is switched on causing a fault signal to be transmitted to the microcontroller. The microcontroller will then switch off the output relay to protect the loudspeaker voice coils from overheating.

Thermistor TH300 is connected to the positive supply rail, adjacent to the collector leg of one of the power output devices. This allows it to sense the collector temperature of the output device. Its impedance when cool is low, typically a few hundred ohms. In the event of a thermal overload (above 110°C), TH300 will go to a high impedance state. This will turn on TR301, which then turns on TR300, causing optocoupler IC300D to switch on, sending a fault signal to the microcontroller. The microcontroller will then switch off the output relay until such time as the unit has cooled down to an acceptable level (80°C or so). TR301 is configured with a small amount of hysterisis (positive feedback) to ensure a clean signal is transmitted to the microprocessor via IC300D.

Optocoupler IC300C is connected in series with the 3 optocouplers mentioned above, producing an overall fault signal. This is so that the microcontroller can determine in which module the fault has occurred, permitting selective control of the output relay for each module in the amplifier.

L924 Amplifier Module Parts List Issue 1.1

L924 Amplifier Module Parts List Issue 1.1

L924 Amplifier Module Parts List Issue 1.1

TP307

Controller Board L925

Contents

- ! **Circuit description**
- ! **Component overlay**
- ! **Parts list**
- ! **Circuit diagrams**

P7 Controller Circuit Description

The Amp controller PCB Panel consists of 6 PCBs.

- Controller PCB
- Display PCB
- Connector PCB
- **Mains Switch PCB**
- 2x Wire Clamp PCBs

Overview

The controller PCB contains the microprocessor and most of the circuitry for controlling the P7 amplifier. The display PCB provides the LEDs and resistors for the simple 7 LED display for the front panel of the unit. The mains switch PCB provides a means of supporting the front panel mounted mains switch. The connector PCB fits on the base of the chassis near the rear panel and provides a means of connecting the 7 amplifier modules to a connector which is then linked to the controller PCB. The connector PCB also provides a means of mounting the rear panel mounted trigger input connector and connecting its signals to the mains controller PCB.

The cable clamp PCBs are used to hold the transformer power cables neatly to the side of the chassis base.

The controller PCB

The controller PCB provides the following functionality

- ! Mains power distribution, switching and soft-start
- Voltage selection for 115/230V operation.
- +5V (for logic) supplies
- ! +22V (for relay and fan) supplies
- Variable speed fan drive
- Relay control for soft starts and sequenced power up/ power down for switch on, switch off and fault conditions.
- ! Heatsink temperature measurement for fan speed control
- ! Transformer Thermal trip monitoring
- Mains supply monitoring for output muting
- Soft start resistor monitoring to prevent soft start resistor overdissipation
- Amplifier module fault status monitoring for module over-temperature, module DC offset, module VI limit
- Output muting relays drive circuit
- Amplifier status display drive circuitry via the front panel mounted LEDs.
- ! Watch-dog failsafe mechanism which activates in the case of microprocessor failure

Mains power distribution, switching and soft-start

The mains input supply is connected directly to the control PCB via SK100. The mains supply is routed through the power relay RLY100 and through the 3 parallel resistors R100, R101, R102. These form a high power rated 50- Ohm resistor that is used to limit the inrush current into the 2 large power toroids. These toroids are mounted beneath the transformer tray at the front of the unit. The 50-Ohm series resistor limits the inrush current to 5A and is allowed to remain in circuit for a few hundred milliseconds after power on. After the power amplifier module electrolytic capacitors have charged to full supply voltage the current through the resistor falls to a low value (which is sensed by the circuitry around IC105 as described below) and the soft start resistor is then switched out of circuit by relay RLY101. This arrangement of power relays ensures that relay RLY101 never switches high voltages and its contacts remain clean.

Voltage selection for 115/230V operation

The control PCB provides a means of configuring the unit for 115V or 230V operation. This is achieved by having 2 connectors marked with the appropriate voltage for each of the units 3 transformers (1 auxiliary transformer which powers the control PCB and 2 large toroids each of which powers 3 ½ amplifier modules). The connectors SK101, SK102 for the aux TX and SK103, SK104 for the Right hand power toroid and SK105, SK106 for the left hand power torroid are configured to place the two primary windings of each transformer in parallel for 115V operation and in series for 230V operation. The arrangement of fuses (6 in total which are all fitted) ensures that each winding has a series fuse when configured in parallel for 115V operation and 1 of each pair of fuses is used to fuse the series configured windings when set for 230V operation. In this way there are 2 parallel fuses for each transformer when set for 115V (to allow twice the current as required). The fuses are time delay types.

C121 is X rated and provides suppression for rectifier switching transients for EMC conducted noise compliance. RC100 is a series RC network to prolong relay life.

+5V supply (for logic)

The auxiliary transformer has 2 secondary windings. These are rectified by full wave rectifiers to form the DC supplies.

The +5V supply is rectified by D101, D102, D105, D106 and smoothed by C102. The supply is then regulated by the 3 terminal 5V regulator REG100. The supply is designed to provide 9.5V DC to th input of the regulator when fed with a nominal 230V. This allows 8V at the input to the regulator (so that it remains within regulation) when fed from 195V mains supply. The regulator is fitted with a heatsink. C103 is provided to eliminate input transients. C107 ensures regulator stability.

+22V supply (for relay and fan)

The +22V supply is formed in a similar manner by D103, D104, D107, D108 and C101. The supply voltage is chosen to give 22V when driven from a mains voltage of 230V. This gives around 24V when the mains supply is at its maximum value (265V). This is due to the relays having a maximum specified input voltage of 24V.

Variable fan speed drive

The fan for the amplifier is required to be very quiet. This is achieved by having the fan speed proportional to temperature. The temperature is measured by the microprocessor (as described below) and when the temperature exceeds a programmed threshold then the fan is switched on at its lowest speed (approx 7V). As the temperature of the unit increases the fan speed is increased until it is operating at full speed (12V). This is achieved by having the microprocessor output a PWM 5V pk to pk square wave on line PWM OUT. The square wave is filtered by R112, C108 to form a DC level. The amplitude of the DC level is thus proportional to the duty cycle that is under microprocessor control. The filtered DC signal is then amplified by the simple 4 transistor amplifier formed around TR100, TR113, TR114 and TR115. The gain of the amplifier is set by R117, R118 to around 6. This ensures

that the PWM_OUT signal duty cycle can move the output of the amplifier over the required range. C104, C113 provide suppression for EMC and C112 provides amplifier loop compensation. The supply to the fan is fused by F101 this fuse limits current in the event of the fan stalling. If the fuse blows the watchdog timer cct immediately switches off the power relays to ensure failsafe condition.

Relay control

The power relay and soft-start relay (RLY100, RLY101) respectively are driven by microprocessor signals MPOWER and MSOFT_ST*. Transistors TR108, TR111 buffer the microprocessor outputs. Diodes D115 and D119 prevent damage to the collectors of the transistors by the inductance of the relay coils at coil switch off.

The power for the relay coils $(+22V_SW)$ is provided through TR116. This transistor is off (hence relays off) when the watchdog circuit detects no microprocessor activity (as described below) or the fan fuse F101 is blown (as described above).

Heatsink temperature measurement

The microprocessor monitors the temperature of the heatsink using the circuitry around TR112. Capacitor C114 is alternately charged through fixed resistor R122 (2K2) and thermistor TH100. The time taken to charge the capacitor is measured by the microprocessor. The ratio of the time taken to charge the capacitor through the 2K2 fixed resistor compared with the time taken to charge the capacitor through the thermistor allows the microprocessor to calculate the resistance of the thermistor. The software is then able to establish the temperature of the thermistor from its resistance.

Three microprocessor lines are involved in this measurement. TREF, TTEMP, C_DISCH.

A measurement cycle proceeds as follows.

C_DISCH goes high to discharge C114. After a delay to ensure C114 is fully discharged C_DISCH then goes Low and TREF is set as an output and goes high. TTEMP is set as an input. This allows C114 to charge through R122. The time taken for C114 to charge to the input high threshold of the micro is measured by timing through input TTEMP.

When the threshold is reached, C_DISCH is again taken high to discharge the capacitor.

After a delay to ensure C114 is fully discharged C_DISCH then goes Low and TTEMP is set as an output and goes high. TREF is set as an input. This allows C114 to charge through TH100. The time taken for C114 to charge to the input high threshold of the micro is measured by timing through input TREF.

When the threshold is reached, C_DISCH is again taken high to discharge the capacitor.

This cycle is repeated continuously and the ratio of capacitor charge times allows the ratio of resistance R122 to resistance TH100 to be measured. The measurement is immune to variation in value of C114, saturation voltage of TR112 and average supply voltage on the 5V rail. The variation of input voltage 1 threshold of the TREF and TTEMP inputs is not compensated for but in practice this is usually found to be minimal. The method should give a measurement accuracy of a few degrees C that is all that is needed for fan speed control.

Transformer Thermal trip monitoring

The main power transformers have thermal trips built into them. These are normally closed and go open when the trip temperature is exceeded. The trips are put in series and pulled to 5V through R131. In the event of 1 (or both) transformer trips going open circuit then line TX_OVTEMP goes high and the microprocessor is then able to power the amplifier down as required.

Mains supply monitoring for output muting

In order to prevent thumps through the loudspeaker when the amplifier is switched off it is necessary to detect the removal of the mains supply so that the amplifier modules can be muted.

This is affected by the circuitry around TR101 and the microprocessor. The AC supply for the 22V rail is sensed by R109. At the positive peak of the mains supply TR101 is turned on and saturates thereby discharging C109. In the event of the AC supply disappearing then C109 will not be discharged and will instead charge to 5V through R132. The time constant R132 . $C109 = 47 \text{m}$ S sets the time taken for line PWROK* to go high. So if the mains supply disappears for around 5 capacitor charge cycles then PWROK* will notify the microprocessor which will then mute the amplifier outputs.

Soft start resistor monitoring

The soft start resistor is used to limit the inrush current into the large power transformers. The resistor is designed to be in-circuit only for the duration of the inrush current at switch on. The resistor must be shorted out by the relay before the amplifier is configured to deliver output current. Also in the event of a fault (e.g. a short across one of the amplifier module reservoir capacitors) then the resistor might be exposed to a situation which might cause over dissipation.

This is avoided by having the microprocessor monitor the voltage across the resistor so that in the event of a fault the amplifier can be switched off before damage to the resistor occurs.

The voltage across the soft-start resistor is monitored by the circuitry around IC105. When voltage is present across the soft-start resistor (only the positive half cycle is sensed) then the opto-transistor is turned on. This discharges C100.

The \overline{RC} time constant R104, $C100 = 220$ mS dictates that line SSPROT^{*} will be low until around ¼ of a second after the voltage across the soft-start resistor has fallen to zero.

Amplifier module fault status monitoring

- Module over-temperature
- **•** Module DC offset
- Module VI limit

The amplifier modules contain circuitry that senses the above fault conditions. The fault status is indicated to the control PCB by means of open collector transistors on each module that are ON when the fault exists.

The means of connecting the fault lines to the control PCB requires explanation.

There are 7 amplifier modules, each of which has 3 fault lines. If these were tracked individually then this would require 21 lines to the control PCB.

In order to reduce the number of lines required then the connections are changed so that the 3 fault lines from each of the are 7 modules are connected in parallel. So that e.g. the VI limit fault line is pulled low when any one of the 7 modules exhibits a VI limit fault. In order for the controller to establish which module has the fault (so that

it can be indicated on the front panel display) each module also provides an address line. A fault occurring on a particular module will cause both the fault line to be low and also the address line. In this way the amplifiers can be monitored by the controller through a total of 10 lines.

The address lines are called:

FAULTn^{*} (where $n = 1$ to 7 as per amplifier module number)

The fault lines are: FLT_DC* to indicate a DC offset error FLT_VI* to indicate VI limit protection FLT_TEMP* to indicate that the temperature of the output transistors has exceeded the 110C trip temperature.

Output muting relays

The muting relays are on the amplifier modules. The relays allow the amplifier to be disconnected from the loudspeaker load. This is required for muting switch on and switch off thumps and in the event of fault conditions.

The relays are driven from the control PCB by the simple open collector transistor drive arrangement formed around TR102, TR104- TR110. The diodes D111-D118 protect the transistor collectors against over voltage spikes occurring when the inductive relay coils are switched off.

The open collector transistors are driven through the 74HC259 type addressable latch. This configuration allows 24 output lines to be provided from 7 microprocessor lines. The outputs of one of the 259s (IC103) are used to drive the muting relay transistors. The remaining packages (IC101, IC102) are used to drive the display LEDs as described below.

Control of the 259s is as follows. Each has 3 address bits S0, S1, S2 which allows one of 8 outputs to be selected, a DATA input which allows a 0 or a $\overline{1}$ to be latched to the output and a GATE input which transfers the signal on DATA to the selected (addressed) output of the package. The GATE input is also used as a chip select to select which of the 3 packages is being controlled. This allows the S and DATA inputs to be connected in parallel on multiple packages.

Amplifier status display

The amplifier status is indicated via the front panel mounted LEDs. IC101, IC102 are used to directly drive the tricolour LEDs which are mounted on the LED PCB. Each channel has a single Tricolour LED. The LED has a red and green LED built in and the third colour (yellow) is produced by having both Red and Green LEDs ON at the same time.

IC101 is connected to the red LEDs and IC102 is connected to the green LEDs.

Watch-dog

The watch dog circuit provides a failsafe mechanism which places the amplifier in a safe (OFF) state in the event of the microprocessor failing or crashing. The circuitry monitors the average voltage on the WATCHDOG line and if it falls outside its required voltage then it removes the power supply to the relays which has the effect of muting the amplifier outputs and removing the power to the power amplifier toroids.

The line WATCHDOG is toggled by the software in the micro. Every time it completes a program loop it toggles the state of the line. This results in a 50% duty cycle signal that is averaged to 2.5V by the filter R114, C110. The voltage is then fed to the window comparator formed around IC104. The network R105, R106 and R107 sets the upper and low thresholds at 75% of 5V and 25% of 5V respectively.

The outputs are open collector and if the filtered WATCHDOG signal exceeds the upper threshold or falls below the lower threshold then the b-e junction of TR103 is pulled low and TR116 is then turned off – which removes the power to the relays.

The filtered WATCHDOG signal can only move outside the window if the WATCHDOG line sits high (or low) continuously. This can only occur if the microprocessor breaks or the software crashes.

This protection scheme also includes the fan fuse (F101). If the fan fuse blows then TR103 gets no base current that also immediately removes the power supply to the relays.

LED PCB

The LED PCB contains the 7 bicolour LEDs and their current limiting resistors. The LED PCB also provides a means of routing the mains switch wiring to the control PCB via the LED PCB to control PCB flexfoil cable.

Connector PCB

The connector PCB provides a means of joining the amplifier modules to the control PCB via the 22way flexfoil cable. The PCB also includes circuitry for the 12V trigger circuit.

The trigger circuit is formed around SK201. The 12V trigger signal is converted to a 5V logic level compatible signal by R200, D200. C201 and C202 provide EMC suppression (since the signal is ultimately routed to the Control PCB which contains a microprocessor). R202 isolates the ground pin of the jack socket from the amplifier ground. This prevents possible ground loop problems with other hifi components connected in the system.

The zener diode clamped signal is limited to 4.7V pk amplitude. This is fed to the microprocessor via line TRIG/RC5

Fault conditions

Fault D.C

When a D.C fault is created on an amplifier all the LEDS turn red accept the module with the fault that flashes green.

Fault V.I

When a V.I fault is created all the LEDS turn red accept the module with the fault which flash red.

Therm fault (amplifier overheating)

When a therm fault is created all the LEDS stay green and the amp module with the fault flashes amber.

Thermal trip (TX overheating)

When a thermal trip is created all the LEDS flash amber, stating that it is a transformer problem.

L925 Controller Board Parts List Issue 1.2

L925 Controller Board Parts List Issue 1.2

L925 Controller Board Parts List Issue 1.2

Control PCB L925CT1_1.2.SCH

Interface PCB L925CT2_1.2.SCH Main Switch and LED Display L925CT3_1.2.sch

A & R Cambridge Ltd Pembroke Avenue Cambridge CB5 9PB Waterbeach

SK300

 $\frac{F}{F}$

FIX300 FIXING HOLE 3.2 FIX301 FIXING HOLE 3.2

DMAIN_SW TP314

RED1 TP300 RED2 TP301 RED4 TP303 RED6 TP305 GRN1 TP307 GRN3 TP309 GRN5 TP311 GRN4 TP310

 $\overline{\Theta}$ Θ $\overline{\Theta}$ Θ

 Θ

 Θ

RED3 TP302 RED5 TP304 RED7 TP306 GRN2 TP308

> GND₃ ϕ DGND_SK302

Transformer Specifications

Contents

- ! **L911TX Power amp 115/230VAC**
- ! **L912TX Aux 115/230VAC**
- ! **L920TX Power amp 100VAC**
- ! **L921TX Aux 100VAC**

Mechanical Assembly

Contents

- ! **General assembly parts list**
- ! **Assembly diagrams Front panel TX tray Rear panel Chassis**

P7 General Assembly Parts List – issue 4

P7 General Assembly Parts List – issue 4

0 10 20 30 40 50 60 70 80 90

All parts can be ordered via spares@arcam.co.uk

Pembroke Ave, Waterbeach, Cambridge, CB5 9PB, ENGLAND TEL: +44(0) 1223 203 203 FAX: +44(0) 1223 863 384